Bunden karnt of Bunden karnt of Relative Relative		Influence of PPF on leaching and subsidence of Gypseaus soils								
Farouk M	I. Muhauwiss <sup>1</sup>	<sup>1</sup> Civil Department/ Engineering College/Tikrit University/ Tikrit,								
		Iraq ahmed h salib43797@st tu edu iq								
Ahmo	ed H. salh <sup>2</sup>	<sup>2</sup> Civil Department/ Engineering College/Tikrit University/ Tikrit,								
		Iraq								
		<u>dr.faroukmajeed@tu.edu.iq</u>								
C	Sypsum soils are fou	nd in various places, including Iraq. The problems created by gypsum								
S	oils are due to the	e presence of gypsum salts, which dissolve in water and affect the								
e t	o collanse	s of the soli over time, causing several problems that can imany lead								
Т	b conapse. This study aims to a	ssess the effect of PPF on the soaked gypseous soil. The tests were								
C	arried out on three	types of gypseous soil with varying gypseous soil rife ceres were								
n	nixed with varying F	PF contents (0, 0.25%, 0.5%, and 1%) at 12 mm length.								
E E	By the compaction r	results, polypropylene fiber increases the optimum moisture while								
r RA	educing the maxim	um dry density. Also, adding (0.5 % PPF) has produced an efficiency								
percentage of 69.9_74.8% in reducing collapsible potential. For the leaching model. The model test results we found through the leaching process showed that the effect fibers in stabilizing the soaked gypsum soils was apparent by preserving the engineering structure and preventing deformations and collapses. Whereas untre- soils became brittle and collapsed under the influence of their weight, this reduced volume by 1795.2 cm3 after 80 days of leaching with water, while the treated soil vol- decreased by only 210.5 cm3.%. The current study's findings point to polypropylene										
						improvement as an environmentally friendly technique for enhancing the engine				
						С	haracteristics of gyp	oseous soil		
						**		Leaching_Gypseaus Soils_Polypropylene Fiber (PPF)_Model Test_		
						Ke	ywords:	Collapse		

#### 1. Introduction

Gypsum soils are distributed in several regions of the world, including Iraq. The problems caused by gypsum soils have been noticed as a result of the presence of gypsum salts, as they cause a continuous change with time in the engineering properties of the soil as a result of the dissolution of these salts upon contact with water, which causes many problems that can ultimately lead to collapse [1]. So, Engineers must treat gypsum soil to reduce its influence on structures. Several strategies increase gypseous soil behavior, such as compaction for shallow layers and injection for deep layers of big or buried structures. also Can use deep foundations like piles by distributing load to stable layers beneath collapsible ones[2] Furthermore, chemical stabilization uses cement, sulfur, a crylate, and sodium silicate to treat collapsible soils. Despite improving soil folding behavior, they can be hazardous and pollute groundwater and soil [2], [3]. However, there are several factors to consider while deciding on a suitable technique, including construction details, economic factors, and the degree of collapse.

Several initiatives to address the soil problem have recently been documented using geofibers for soil stabilization and improvement. Due to the low cost and ease of deploying technology, the light weight of the additive (i.e. geofibres), and history of successful cases, geofibers are popular among practitioners. Geofibers improve shear modulus, liquefaction resistance, particle entanglement, and load-bearing capacity in granular or non-cohesive soils [4].

Geofiber These are typically fibers integrated into soils to form a perfect reinforcement system for fixing slope failure, reinforcing pavement subgrade, stabilizing foundations, and enhancing backfill for retaining walls. By working well with the soil already there, geofibers help create a soil reinforcement system with much better engineering features [5].

Fibers available for use in construction can be classified as natural fibers (e.g., coir fibers, jute fibres, etc.), synthetic fibers (e.g. polypropylene fibers, polyester fibers, etc.), and waste fibers (old/used tire fibers, used plastic fibers, etc.)(nonhazardous type) materials[6]. Previous research has shown that using natural fibers in poor soils can improve the soil's mechanical behavior even with a modest amount of fiber. Waste materials and synthetic fibers boost soil strength by enhancing friction interlocks and bonds between soil particles[7]. Furthermore, fiber can make construction more cost-effective projects and environmentally friendly. Because fibers may be derived from waste goods like old tires, used plastic, etc., their utilization can help resolve waste disposal difficulties; otherwise, these wastes can occupy a large amount of landfills[8]. Several researchers have looked at the shear strength of fiber-reinforced soils and found that it significantly improves the soil's shear strength and ductility. Specifically, fibers boost the soil's peak shear strength while the postpeak decrease in shear strength is limited [9].

According to standard Proctor tests, adding jute fibers at a rate of 0–1% by weight of dry soil raises the optimal water content of clay with low plasticity and lowers the maximum dry unit weight [10]. The modified Proctor tests carried out by (AbdulRahman et al.) indicate that the presence of 1% polypropylene fiber (PPF) by weight of dry soil causes the maximum dry density of reinforced gypsum soil to decrease[11]. Also (Ali1a et al.) found that the maximum dry density of reinforced soil with PPF slightly decreased by 2.8% [12].

[13] was performed **Oedometer** tests investigated the effect of glass fibers on collapsible soil. Glass fiber with 0, 3, 4, 5, and 6 % was utilized to treat laboratory remolding soil. The study shows that glass fiber treatment reduces soil collapse. (AbdulRahman et al.) were evaluated (PPF) effect on gypsum soil with a 39% gypsum concentration and 6 mm fiber lengths. The results of the odometer test are shown for the gypseous soil after mixing with PPF. The collapse potential was significantly reduced, from 13.9% to 0.96% for (0 to 1%) fiber content [11].

[14] were evaluated the possibility of using fibers to reduce collapsible soil potential alone or in conjunction with Portland cement. Polypropylene fibers in various ratios (0, 0.1, 0.2, 0.5, and 1 percent) lengths of 12 mm were mixed with a cement soil mixture. The cement content is available in three concentrations (0. 1, and 5%). Odometer tests were carried out to determine the effect of a fiber and cement mixture on the collapse characteristics of treated collapsible soil. The results showed that increasing the fiber content from 0% to 1% with 0% cement content reduced the collapse potential from 13.68% to 6.83%. Also, fibers can be used to reduce cement content while maintaining the same results. with а combination of 0.2 percent fibers and 1 percent cement being as effective as using 5 percent cement for treatment without fibers in terms of CP reduction.

Though previous studies have shown that geofiber is a sustainable material for improving the geotechnical properties of a wide variety of soils, applying geofiber to treat gypseous soil is A little bit. So, this research looks at what

#### Volume 11| October, 2022

#### ISSN: 2795-7640

happens to the properties of gypseous soil when polypropylene fiber is added, especially when the soil is wet, by carrying out tests in the lab, such as the collapsibility tests and the leacgine model test.

# 2. Materials and methods 2.1 Soil

The soil used in this research was collected from three locations in the Salah-Aldin Governorate and was representative of three types of disturbed natural gypseous soil. The samples were taken from a depth of 0.5 to 2 meters below the earth's surface. The first one was brought from Tikrit University, which has a gypsum content (56%) and is defined as (soil 1). The second variety is from AL'Dour, has a medium gypsum content (36%), and is known as (soil 2). Finally, the third is from Al 'Alam, but its low gypsum content (21%) is referred to as (soil 3). Fig (1) displays the soil samples' grainsize distribution curve, and The USCS categorizes these soils as "poorly graded sand," which is the lowest soil quality level (SP). Table (1) to Table (3) presents gypseous soils' physical and chemical properties and the test standards



Figure 1: The grain-size distribution curve

Property	Specification		
Grain size distribution	ASTM D422 [15]		
Specific gravity	ASTM D854 [16]		
(LLand PL)	BS 1377:2A-ASTM D4318 [17][18]		
Compaction test	ASTM D1557 [19]		
Field density	ASTM D1556 [20]		
Chemical tests	BS 1377-3 [21]		

**Table 1:** Gypseous soils tests with their Specification

<b>Table 2:</b> Physical properties of gypseous soils								
Soil	Specifi	Atterberg's		Grain	size	Compaction test		γf
symbol	С	limits	limits distributio				KN/m <sup>3</sup>	
	gravity	n						
	(Gs)							
		LL%	PL%	Cu	Сс	$\gamma$ d max	0.M.C %	
						kN/m <sup>3</sup>		
Soil 1	2.36	92.2	N.P-SM	4.86	1.11	17.65	11.75	12.17
Soil 2	2.46	34.2	N.P-SM	5.10	1.07	17.49	13.31	13.34
Soil 3	2.51	32.9	N.P-SM	4.63	0.84	18.91	10.45	14.05

# Table 3: Chemical properties of gypseous soils

properties	Soil1	Soil2	Soil3
Total soluble salts (T.s.s)%	64.41	37	25.31
Organic matters (0.M)%	0.015	0.048	0.091
PH value	7.88	7.81	7.78
Gypsum content %	57	36	21

#### 2.2. Polypropylene Fiber (PPF)

Polypropylene fiber is a polymeric fiber and is one of the most recent members of the rapidly growing thermoplastic polymer family are prepared using the melt spinning technique, which consists of two manufacturing stages: (1) extrusion of a fiber and (2) subsequent thermal and mechanical stretching of the fiber. In this process, a viscous fluid is extruded through a multihomed die or spinneret, forming a fine-diameter fiber [22].

Table (4) shows the properties of the (PPF) which was brought from the Sika Company and is depicted in plate (1).

property	value				
Colour	transparent fibers				
Density	0.91 g/cm3				
Length	12mm ± 1mm				
diameter	0.032 mm				
Tensile strength:	600-700 Мра				
Elastic Modulus	3.000-3.500 Mpa				
Elongation	20-25 %				
Chemical Base	100% virgin polypropylene				
Melt point	160°c				
Ignition point	365°c				

		<i>c</i> 1	1 (1)	
Table 4: The	properties	of polyp	ropylene fibei	



Plate 1: Polypropylene fiber (PPF) used in the present research

# 3. Experimental program

# **3.1. Sample Preparation**

The soil was prepared using samples passing through sieve No.4, then oven dried for 48 hours at 45 °C., then moved to a mixing container. The required amount of water is added to the specimen, and the batter is then carefully mixed by hand to ensure that it is homogeneous.

For fiber-reinforced samples, at this point, the required percentage of fiber is added to the wet

soil, expressed as a percent of the total dry weight of soil, and manually mixed into the wet soil in small increments. Because it was observed that if the fibers were mixed into dry soil, it would cause segregation or the floating tendency of fibers, then it was mechanically mixed. Before the tests, the prepared mixtures were kept for 24 hours in airtight bags so that the moisture would be evenly spread throughout the sample.

# **3.2 Testing Program3.2.3 Co3.2.1 Compaction test**OedomeMaximum dry density and optimal moistureaccordancontent for compacting the three soil types weresoil's co

content for compacting the three soil types were determined using a modified proctor test (ASTM D1557). it was dried at 45 °C for 48 hours, eliminating the possibility of water crystallization being lost from the gypsum, allowing an accurate determination of its moisture content.

#### 3.2.3 Collapse tests

Oedometer devices were conducted in accordance with (ASTM D5333-03)[23]. The soil's collapse potential (CP). was evaluated using a test proposed by (Knight, 1963) and known as the collapse test or the Single Oedometer Test (CP)..The severity of the collapse potential indicated is shown in Table 5.

Johla F. Callanca idanti	fication (aftar )	lonninge I one	$\frac{1}{100}$
able 5: Collapse Ideliu	iicatioii (aitei )	emmigs, j. and	1 KIIIgiil, 1973/124
······································			

Severity	No problem	Moderate	Trouble	Severe	Very severe
CP (%)	0-1	1-5	5-10	10-20	>20

# 3.2.4 Leaching Model Test

The impact of wetting on the behavior of gypsum soil's pristine surface was studied in a model experiment. The model consists of the following parts, As can be seen in Plate 3.6

- 1. The glass container is 150mm, 250mm, 300mm in dimensions, and 10mm in thickness. To show the actual situation of how to drain the water from gypsum soil in sit., we made holes in the model's base.
- 2. For a representation reality of the gypsum soil's exposure to rainwater, irrigation, or other water sources, the container's water supply faucets must be located at the container's top and connected to a water tank until the water reaches the model's surface.
- 3. A gravel layer (7) cm thick is placed on the container's bed to make the water dissipate. then (3) cm thick layer of graded sand is put on top of the gravel layer to keep soil from getting through the holes in the bottom container and to act as a filter for the gypsum soil.
- 4. To prevent the soil specimen from shifting and to prevent the filter from mixing with the gypsum soil, a layer of filter paper was placed on top of the previous layers.

It was decided to create two model assessments. The first model was evaluated on untreated gypsum soil (1), and the second was evaluated on the same soil treated with 0.5% of the dry weight of the PPF. Both untreated and fibertreated soil samples were generated with the same dimensions (150 mm x 150 mm x 250 mm) and a density equal to 83% of the maximum dry unit weight. The soil was compacted inside the model to a total thickness of (15 cm) using a hammer, The specimen was compacted into five equal layers. Each layer is 3 cm thick. The changes that will occur to the gypsum soils in the model are checked every (7,15,22, 31, 38, 50,60,70, and 80) days .

# 4. Results And Discussion

# 4.1. Compaction tests

Figures (2) and (3) show the changes in maximum dry density and optimum moisture content (OMC) with PPF, respectively. It has been noticed that the maximum dry density drops and the optimal moisture content rise with the increase in the gypsum content of the soil.

Results showed that as PPF concentration was raised, maximum dry density decreased and OMC increased. the density of ppf-treated soil 1 decreased from 17.65 to 17.19 kN/m3, and the (OMC) increased from 11.75 to 12.85% when PPF content increased from 0 to 1%. While in PPF-treated soil (2), it is seen that with a rise in ppf content from 0 to 1%, the ( $\gamma$ dmax) decreases from 17.49 to 16.94 kN/m<sup>3</sup> and the (OMC) increases from 13.31 to 14.18 %. For soil (3), increasing the PPF content from 0 to 1% reduces density from 18.91 to 18.37 kN/m<sup>3</sup> while increasing the (OMC) from 10.45 to 11.54%.

Increases in fiber content are related to decreases in dry density, as demonstrated above. Because fiber has a lower specific gravity value (0.91 gm/cm3) than some of the soil particles it replaces [12].



Figure 2: Maximum dry density of PPF-treated soils



Figure 3: Optimum moisture content of PPF-treated soils

# 4.2 Collapsibility of PPF-Treated Soils

Collapse behavior in gypseous soils was evaluated using a single oedometer. The results of collapse experiments conducted on three different gypseous soil types are summarized in Table 6; the data show the relationship between effective stress (log v) versus the void ratio (e). The highest value of collapsible potential for soil with a high gypsum content (soil 1) was 6.75%, and it is classified as (Trouble)by (Jennings, J. and Knight, 1975). Soil (2) had a collapse potential of 4.8%, while soil (3) was only 3.3%, That was categorized as (Moderate) of collapse. The collapse test results for three varieties of PPF-treated gypsum soil are depicted in Figure (4).

The addition of 0.5% PPF content reduced the collapse potential of soil (1) from 6.875% to 2.03%. representing а 69% efficiencv percentage in decreasing collapse potential. and the soil classification was changed from problem to moderate. The collapse potential of soil 2 was decreased to 1.3% after being treated with 0.5% PPF, with a 72.9% efficiency percentage, while the collapse potential of soil 3, which had a low gypsum concentration, was reduced to 0.83% and reached the "No Problem" level. with a 74.8% efficiency

#### Volume 11| October, 2022

percentage in lowering the collapsible potential. Figure (5) shows the effect of gypsum concentration on collapse potential.

The presence of fibers increases the cohesiveness of soil particles and provides

another type of link that resists the inundation of collapsible soil. As a result, limits volume change by preventing soil particles from sliding relative to one another, which may be attributed to a reduced collapse potential [14][25]

	Soil 1	Soil 2	Soil 3
PPF (%)	Collapse potential	Collapse potential	Collapse potential
	%	%	%
0	6.75	4.8	3.3
0.25	3.808	2.69	1.03
0.5	2.03	1.3	0.83
1	2.34	1.375	1.18

**Table 6:** Summary of the results of the Collapse test



Figure 4 : Effect of PPF content on collapse potential



Figure 5: Influence of gypsum content on collapse potential for PPF-treated soils

# 4.3 Leaching Model Test

Gypseous soils have a high bearing capacity, little settlement, and negligible creep, As mentioned earlier, these are all desirable engineering features. However, once wet, the structure becomes weak and it begins to fall due to the arrangement of soil particles, which may cause it to collapse under the effect of the initial and without any extra external weight loads[26]. As a result, local soils can be improved to the point where they can be utilized in a certain project without problems significant in the future . Plate (2) depicts a model that was fabricated to investigate PPF to stabilize the soaked gypsum soil.

After the model has been set up, water is poured over both the treated and untreated gypsum soil from above, and the soil remains submerged in water for the test duration. Through this process, the water will drain from the holes in the model's base and may be washed the soil from the gypsum. Time-Volume variation during each testing period is depicted in Figure (6) for both the treated and untreated models.

During the initial week of testing, the untreated specimens showed voids and deformations. A contrast to this is that the treated specimens showed no visible deformation while still maintaining its original form, as can be seen in **Plate (3)**.

The voids and deformations on the untreated model's upper and front surfaces widened after 22 days of tests, and the deformation was shaped as a semicircle, as shown in **Plate (4)**. Due to this, the volume of untreated soil in the model reduced from 5625 cm3 to 5214.1 cm3

after 0 and 22 days, whereas the volume of treated soil did not change.

Submerging the specimens in water causes the holes and deformations in the untreated model to increase. The model's top surface develops fractures and voids after being examined for 31 days. There is a clearer indication of this trend after 38 days of testing, at which point the volume has decreased to (4987.02 cm3 and 4683.33 cm3) after 31 and 38 days of the test,

**Plate (5)** display the testing results after 70 days, It can be observed that the untreated gypsum soil experienced a continuously increasing collapse. also, deformation and cavities showed up on top of the model, and the soil became brittle and loose, causing a drop in volume to 3938.83 cm3. This is because the gypsum dissolves, removing the cementation between the soil particles, and since the wetting process is continuous, the gypsum dissolves continually, increasing the structural collapse due to the breaking of the soil particle connection [27]. At the end of the examination period, which lasted for 80 days, the volume change stabilized. the untreated model's volume reduced to 3829.8 cm 3, whereas the treated model's volume decreased from 5625 cm 3 to 5414.5 cm 3 At (0\_80) days, and it was noticed that the soil decreased by one level due to the fiber reinforcement in the soil as illustrated in

respectively. Whereas the Fiber-treated soil experienced reduced volume change over the same examination periods, some gaps did occur in the model's front surface while the soil structure was preserved from deformations.

After 50 days of examination, the untreated soil began to collapse, as represented by the fall of some part of soil from the sides of the model into the holes formed in the specimen

**Plate (6),** The final improvement in the rate of volume for treating gypsum soils with PPF was 88.2%.

Through this examination, we found during the soaking process of the specimens that water did not easily permeate treated soil. It stops for more than one day at the soil's surface This is because the PPFcloses the flow channels and decreases the voids between the soil particles. In addition, provides the type of bond that resists the inundation of collapsible soil and adds to the cohesion of the soil particles. It also wraps the particles so that water does not soak up through the soil. This was observable from the model's solidity and cohesion [11]. This is found to be contrary to the case of untreated soil where, over hours, the water was completely penetrating the model due to the many gaps and voids formed by gypsum dissolution.



Plate 2: (a) PPF-treated gypsum soil 1 (b) natural gypsum soil 1







Front view



Top view **Plate 3:** The model's test after **7** (days) (a) PPF-treated gypsum soil: (b) natural gypsum soil



**Front view** 





Plate 4: The model's test after 22 (days) (a) PPF-treated gypsum soil: (b) natural gypsum soil



#### ISSN: 2795-7640

#### Volume 11| October, 2022





Top view Front View



Plate 5: The model's test after 70 (days) (a) PPF-treated gypsum soil: (b) natural gypsum soil

#### ISSN: 2795-7640





Top view

# **Front view**



Plate 6: The model's test after 80 (days) (a) PPF-treated gypsum soil: (b) natural gypsum soil



### 5. Conclusions

This research has studied the effect of (PPF) on leaching gypsum soil. The obtained results can lead to the following conclusion.

- 1. Maximum dry density drops from 18.91 to around 16.94 KN/m3 as PPF concentration rises, whereas optimum moisture content rises from 10.45% to 14.18%.
- 2. By adding 0.5% PPF to gypsum soil, the collapse potential is reduced by more than 69.9-74.8%
- 3. The model tests showed the fibers' efficiency by stabilizing saturated gypsum soil. Compared to untreated soil, PPF-treated soil had less deformations, gaps, and volume changes. Untreated gypsum soil lost 28% of its volume after 80 days, while PPF-treated soil lost about 28% of its volume.
- 4. (PPF) is cheap and efficient, so it may be used to enhance wide regions at a decent cost. On the other hand, it is environmentally friendly because it can solve significant waste disposal problems.

#### **References:**

- Q. A. J. Al-Obaydi, "Studies in geotechnical and collapsible characteristics of gypseous soil," Unpubl. M. Sc. Thesis, Civ. Eng. Dep. Coll. Eng. Al-Mustansyria Univ. Baghdad, Iraq, 2003.
- [2] M. Ayeldeen, A. Negm, M. El-Sawwaf, and M. Kitazume, "Enhancing mechanical behaviors of collapsible soil using two biopolymers," J. Rock Mech. Geotech. Eng., vol. 9, no. 2, pp. 329–339, 2017, doi: 10.1016/j.jrmge.2016.11.007.
- [3] I. Chang, J. Im, and G.-C. Cho, "Introduction of microbial biopolymers in soil treatment for future environmentallyfriendly and sustainable geotechnical engineering," Sustainability, vol. 8, no. 3, p. 251, 2016.
- M. H. Maher and R. D. Woods, "Dynamic response of sand reinforced with randomly distributed fibers," J. Geotech. Eng., vol. 116, no. 7, pp. 1116–1131, 1990.
- [5] D. U. K. M. CHATRABHUJ,

"STABILIZATION OF SOIL BY USE OF GEOMEMBRANE AND GEOFIBERS Geomembran," Int. Res. J. Eng. Technol., vol. 07, no. 09, pp. 2511–2515, 2020.

- [6] S. K. Shukla, "Fundamentals of fibrereinforced soil engineering". Springer Singapore. 2017.
- [7] M. Mirzababaei, A. Arulrajah, A. Haque, S. Nimbalkar, and A. Mohajerani, "Effect of fiber reinforcement on shear strength and void ratio of soft clay," Geosynth. Int., vol. 25, no. 4, pp. 471–480, 2018.
- [8] S. K. Shukla, "Geosynthetics and ground engineering: sustainability considerations," International Journal of Geosynthetics and Ground Engineering, vol. 7, no. 1. Springer, pp. 1–3, 2021.
- [9] D. H. Gray and H. Ohashi, "Mechanics of fiber reinforcement in sand," J. Geotech. Eng., vol. 109, no. 3, pp. 335–353, 1983.
- [10] P. Aggarwal and B. Sharma, "Application of jute fiber in the improvement of subgrade characteristics," in Proc of int conf on adva in civ eng, Trabzon, Turkey, 2010, pp. 27–30.
- [11] S. M. Abdulrahman, M. Y. Fattah, and E. A. Ihsan, "Influence of plastic fiber on the geotechnical properties of gypseous soil," Int. J. Eng. Trans. B Appl., vol. 34, no. 2, pp. 367–374, 2021, doi: 10.5829/IJE.2021.34.02B.08.
- [12] M. Ali1a, M. Aziz, M. Hamza1c, and M. F. Madni3d, "Engineering properties of expansive soil treated with polypropylene fibers," Geomech. Eng., vol. 22, no. 3, pp. 227–236, 2020.
- [13] N. Bakir, K. Abbeche, and G. Panczer, "Experimental study of the effect of the glass fibers on reducing collapse of a collapsible soil," Geomech. Eng., vol. 12, no. 1, pp. 71–83, 2017.
- [14] M. Ayeldeen, W. Azzam, and M. G. Arab, "The Use of Fiber to Improve the Characteristics of Collapsible Soil Stabilized with Cement," Geotech. Geol. Eng., pp. 1–13, 2021.
- [15] ASTM D422-63, "Standard Test Method for Particle-Size Analysis of Soils (Withdrawn 2016)," ASTM International, West Conshohocken, PA, 2007.

- [16] ASTM D854-14, "Standard Test Methods for Specific Gravity of Soil Solids by Water Pycnometer," ASTM Int. West Conshohocken, Pa. doi, vol. 10, 2014.
- [17] BS 1377-2, "Methods of test for soils for civil engineering purposes," Classification tests. British Standards Institute London, UK, 1990.
- [18] ASTM D4318, "Standard Test Methods for Liquid Limit, Plastic Limit, and Plasticity Index of Soils.," ASTM International, West Conshohocken, PA., 2017.
- [19] ASTM D1557-12e1, "'Standard Test Methods for Laboratory Compaction Characteristics of Soil Using Modified Effort (56,000 ft-lbf/ft3 (2,700 kNm/m3))," ASTM International, West Conshohocken, PA., 2012.
- [20] ASTM D1556/ D1556M-15e1, "Standard Test Method for Density and Unit Weight of Soil in Place by Sand-Cone Method," ASTM International, West Conshohocken, PA., 2015.
- [21] BS 1377-3, "'Methods of Test for Soils for Civil Engineering Purpose," .Part 3: Chemical l& Electrochemical Tests., 1990.
- [22] A. V. Galanti and C. L. Mantell, Polypropylene Fibers and Films.Springer Science+Business Media New York. 1965.
- [23] ASTM D5333-03, "Standard Test Method for Measurement of Collapse Potential of Soils (Withdrawn 2012)'.," .ASTM International, West Conshohocken, PA., 2003.
- [24] K. Jennings, J. and Knight, "A guide to construction on or with materials exhibiting additional settlement due to" Collapse" of grain structure," 1975.
- [25] A. Ashour, M., Abbas, A., Altahrany, A., Alaaeldin, "Modelling the behavior of inundated collapsible soils.," Engineering Reports.2020;e12156. Wiley online library.com/journal/eng2 1of14., 2020.
- [26] W. A. Zakaria, "Intrusion of Geomesh in Gypseous Soil Under Single Footing," Int. J. Eng., vol. 33, no. 9, pp. 1731–1736, 2020.
- [27] N. M. Toma and M. T. Al-Hadidi, "The effect of soaking and wetting on the properties of the gypsum soil treated with polyurethane," Assoc. Arab Univ. J. Eng.

Sci., vol. 29, no. 2, pp. 1–8, 2022.